

Automatic Load Shedding calculated with Genetic Algorithms – DAC-CMAG

Michelle Guichon, Magdalena Melo, Ana Carolina Nieto, Mario Vignolo, Nicolás Yedrzejewski

Abstract— This paper presents an optimization tool based on Genetic Algorithms, DAC-CMAG (Automatic Load Shedding Calculated Through Genetic Algorithms), developed in Matlab and applied to the calculation of load shedding in Electric Power Systems. This application calculates the optimal load shed necessary to eliminate overloading of any series element of an electrical network. It includes a module that runs DC load flow to calculate the power flow for each branch or transformer and verifies there are no current violations in any equipment. The results are analyzed using this tool applied to the calculation of optimum load shed required for the worst contingencies in the 500kV power system of Uruguay.

Index Terms—DC load flow, load shedding, Genetic Algorithm

I. INTRODUCTION

IN electric power systems, electric energy demand is in general concentrated in cities and towns. On the other hand, generation may be far from any city, often responding to the type of primary energy source used by generating plants. The clearest example is made up of hydroelectric power plants that use the reservoir created by a river dam, transforming the gravitational potential energy of water to drive a turbine and generate electricity. This resource ...

To transport energy from points of generation to demand, high and extra high voltage transmission networks are used. In Uruguay, high and extra high voltage comprises voltages up to 150 kV and 500kV respectively. Because of the importance of the transmission network, the power system is in general designed and built to be reliable and allow system operation even in the absence of one or more constituent elements, namely: lines, underground cables, transformers, etc. However, there are many contingencies for which it is necessary to disconnect part of the load to ensure the stability of the entire system and the integrity of the equipment. In most cases, disconnection should be performed so rapidly that it is possible only automatically, having chosen the stations and conveniently disconnections in advance.

The project includes the study of the behavior of genetic algorithms (GA) to optimally calculate the least amount of load that is necessary to disconnect from the electrical power system after a contingency has occurred, to ensure that any equipment be loaded beyond its load limit in an emergency.

II. DC LOAD FLOW

DC load flow is implemented considering the common simplifications to load flow, namely:

- differences between bus angles sufficiently small:
 $\cos(\delta_i - \delta_j) = 1$
 $\sin(\delta_i - \delta_j) = (\delta_i - \delta_j)$
- shunt susceptance and series resistance not considered
- every bus in the system with constant 1pu voltage

The final equation of power flow for any series element is:

$$P_i = \sum_{n=1}^N B_{in} * (\delta_i - \delta_n)$$

Where B_{in} is the inverse of the series reactance of the branch between bus i and bus n .

III. MODELING OF THE ELECTRICAL NETWORK

The electrical system is modeled in a simplified manner, using only the parameters necessary for the implementation of DC flows. The electrical system components included are: generators, lines and / or cables, transformers.

- The generators are modeled as a typical PV bus in any load flow, with the active power and voltage defined as known data. In this case the voltage, as in the rest of buses in DC load flows is 1 pu.
- In transformers, series resistance and the magnetizing branch are neglected leaving only the series reactance
- The load buses are modeled as constant active power regardless of the reactive power
- In the line model, series resistance, shunt conductance and shunt susceptance are neglected leaving only the series reactance.

IV. GENETIC ALGORITHMS

A. Introduction

Genetic algorithms are adaptive methods generally used in search and optimization data problems, based on sexual reproduction and the principle of survival of the fittest.

B. Adjustment function (fitness)

The fitness in the nature of an organism is defined as the probability that the organism survives to reproductive age and reproduces. The fitness function can be think as a numerical measure of profit, utility or goodness of a solution that can be maximize.

C. Operators

The simplest form of genetic algorithms involves three types of operations:

- Selection: select people in the population for reproduction. The selection of an individual is related to its adjustment value. The biggest adjustment has an inhabitant the more likely is to be chosen for reproduction. The easiest to create is a roulette wheel where each individual in the population is assigned a portion of the wheel, proportional to its fitness value. The better fitness has an inhabitant, the greater the portion of the wheel to be assigned, ergo, the more likely is to be chosen in the draw.
- Crossover: After being selected, individuals are crossed to produce offspring that are inserted into the next generation. This operator randomly chooses a crossover point and exchanges the subsequence before and after the crossover point between individual parents to form children.
- Mutation: This operator randomly changes one bit of the inhabitant given by the probability of mutation.

V. FITNESS FUNCTION

It must be define a fitness function that qualifies each inhabitant of the population. After that, the population can be sorted by ranking. The first thing to take into consideration is the load connected to the network. It is a desire to have connected load as much as possible. Therefore, the function must reward inhabitants with more load connected. For this, two variables are created to quantify the load remains connected, the first is the amount of load remains connected (*Pconnectada in the software*), the second is the number of buses that remains on service (*cantbarras in the software*). The fitness function is implemented to be an increasing function in these variables:

$$fitness \propto Pconnectada \times cantbarras$$

Another variable to consider is the overloaded equipments. The main target is to eliminate every current violation. Therefore, the function fitness must assign smaller fitness values for the most overloaded network.

In this case, two variables are defined to represent how overloaded is the network: *sob*, number of overloaded branches (or transformers) and *Smax*, is the ratio between the line load of the most heavily loaded line and the thermal capacity of the line. The following equation for the fitness function is proposed.

$$fitness = \begin{cases} Pconnectada^3 \times cantbarras^3 \times (S_{max} \times 100)^9; sob = 0 \\ \frac{1}{\left(e^{\frac{sob}{10}}\right)^2} \times \left(\frac{Pconnectada^3 \times cantbarras^3}{S_{max}^2}\right); sob \geq 1 \end{cases}$$

Where *sob*, is the number of overloaded branches in the system.

This function accomplishes all the requirements. For further details in the development of the function, see [1].

VI. MAIN PROGRAM

This section discusses the implementation of major program that calculates the optimal load shedding for the various contingencies that may occur in the network using tools DC power flow and genetic algorithms.

Input and data procesing

The network data is read from an Excel spreadsheet as explained below. In the first page, called *Barras*, is the list of stations with their respective power loads and generation, which expressed in MW. In some cases, depending on user requirements, there would be convenient to leave certain fixed stations. This option is included on the first page where the user must put a 1 for allow the station of interest to participate in the load shedding and a zero in those buses not allowed to participate. In the second and third sheet there are the line and transformer data. They contain the impedance of each line, expressed in pu, and up to 2 maximum current limits (A and B), expressed in Amper. Also expresses the voltage base.

The network data is read when the file is opened through the graphical user interface of the program. The function *devuelveDatos.m* is who is responsible for processing them for later use in the rest of the program.

Then, functions *DevuelveXY.m* and *armaMatrizA.m* are executed. The first, return arrays *X* and *Y* corresponding to the series impedance and admittance of lines and transformers. The second returns a matrix with a dimension $N \times B$ for a network with *N* lines *B* buses. For line *i*, $a_{ij}=1$ when *j* is the first bus of the line and $a_{ij}=-1$ for the second bus. Matrix *A* completely describes the topology of the network and is independent of the particular values of line parameters. Once the angles of the buses are calculated (vector *Ang*), the power flow throw the line from bus *i* to *j* is:

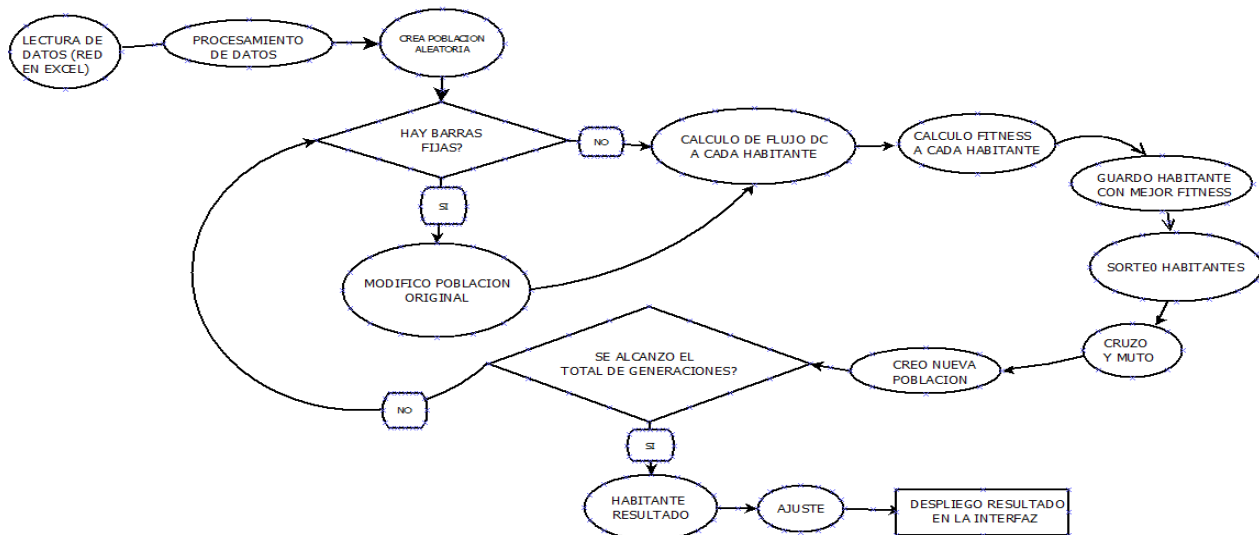
$$P_{ij} = A \times Ang \times Y$$

Main program

Initially, the program creates a certain amount of individuals to form the initial population. Each inhabitant represents a possible combination of substations to disconnect. Each individual is represented by a vector, with length equal to the number of substations in the network.

Each vector element is associated with a single substation and can take only two possible values, 0 or 1. The value 1 indicates that the substation remains in service and is not disconnected in that combination. The value 0 indicates that the substation is part of the load shedding for that combination.

Ultimately, each inhabitant represents the state of all network stations in the post-contingency situation. An iteration start, where in each step the program creates a new generation doing the following:



1. The program checks for fixed stations. If so, an amendment is created in the population by setting the value 1 in positions corresponding to stations that must remain connected in every inhabitant.

2. Next, it calculates the fitness of each inhabitant of the population. To do this, function *flujoDChabitante.m* calculates a DC power flow to find the angle of every bus. In a common implementation of a DC power flow, a previews balance between load and generation is mandatory so there is no need of a slack bus like in AC power flows. However, in this case every inhabitant has different load connected so a correction in generation must be done before running a DC power flow. For this purpose, the first bus entered in the list of buses will be considered to state the balance.

3. Function *elem.m* calculates the node admittance matrix, *Ybus*. *flujoDePotencia.m* calculates the active power en every series element using matrices *A* and *Ybus* explain above.

4. *Sobrecarga.m* calculates the overloaded lines and transformes.

5. *fitness.m* calculates the fitness of every inhabitant and place in matrix *habmax* the one with best fitness for every generation.

6. To create the next generation, inhabitants are drawn, by *sorteo.m* function which uses *ruleta.m* (*ruleta.m* function is based on the selection operator of genetic algorithms explained above).

7. Function *cruzaymuta.m* cross and mutate the inhabitants drawn, creating a new population.

This process is repeated until the total number of generations is reached. The inhabitant of best fitness of all generations is taken as a partial solution.

For this inhabitant, function *ProgramaPrincipalAjuste.m* implements a final adjustment to the partial solution to ensure that the combination selected do not disconnect excessive and unnecessary load. The setting procedure is described below:

- The program goes through every bit of the inhabitant changing each zero by one and re-run the DC power flow. In each test, if the new inhabitant has no overloaded

elements is stored in an array. The resulting matrix contains all the changes successful.

- The inhabitant of the matrix with lower disconnected load is chosen and the rest are discarded.
- With this new individual, the process is repeated.
- When every additional change is unsuccessful, the adjustment is terminated.

The adjusted inhabitant is considered the best solution found. Through the user interface, the program shows the final combination of station to be disconnected, the active power associated and the most overloaded line or transformer expected if the solution suggested is implemented.

VII. APPLICATIONS IN THE TRANSMISSION NETWORK OF URUGUAY

This chapter analyzes the behavior of the tool developed in this project to calculate the necessary load shedding for the most severe contingencies in the 500kV system of Uruguay.

The rate chosen is the thermal capacity the equipment supports for an hour and no more, which is appropriate in this regime. It considers a peak demand for the summer and winter, 2012.

It works with a mutation probability of 0.1%, 70% for crossover, population size of 1000 inhabitants and initially with 100 generations. This can vary according to the number of lines that may be overloaded.

PAL500-MVA500 and BRU500-MVB500 double contingency for summer peak

The following table shows the lines that are overloaded and the percentage of overload without load shedding:

| Initial Bus | Final Bus | Current (A) | Overload (%) |
|-------------|-----------|-------------|--------------|
| ACO150 | MVB150 | 951.603 | 183.001 |
| BAY150 | PAL150 | -1101.14 | 229.418 |
| BAY150 | TRI150 | 559.068 | 155.348 |
| COL150 | ROS150 | 281.748 | 117.308 |
| COL150 | JLA150 | 567.059 | 136.666 |

| | | | |
|--------|--------|----------|---------|
| CON150 | COL150 | 928.72 | 258.063 |
| DUR150 | FLO150 | 1357.076 | 220.362 |
| EFI150 | SVA150 | 479.354 | 199.583 |
| FBE150 | MER150 | 975.182 | 203.175 |
| FLO150 | PRO150 | 1253.045 | 203.469 |
| JLA150 | LIB150 | 567.059 | 191.581 |
| LIB150 | EFI150 | 506.528 | 140.749 |
| MER150 | NPA150 | 1008.242 | 419.79 |
| NPA150 | CON150 | 931.804 | 224.573 |
| PAL150 | TRI150 | 1671.054 | 348.158 |
| PAY150 | YOU150 | 575.913 | 138.8 |
| PRO150 | MVA150 | 1253.045 | 203.469 |
| ROD150 | ACO150 | 1024.68 | 213.488 |
| ROD150 | MVB150 | 1210.878 | 195.888 |
| SAL150 | PAY150 | 741.251 | 154.437 |
| SGU150 | SAL150 | 890.733 | 185.581 |
| SJA150 | FBE150 | 1009.11 | 163.859 |
| TER150 | BAY150 | -923.123 | 149.337 |
| TER150 | DUR150 | 1421.026 | 197.43 |
| TRI150 | ROD150 | 2192.466 | 228.396 |
| SGU500 | SGU150 | 306.131 | 160.677 |
| SJA500 | SJA150 | 302.733 | 158.894 |
| PAL500 | PAL150 | 832.608 | 277.331 |

To clear the overloads of the network the program calculates that 858 MW to be disconnected by shedding the following (all at 150kV):

| | | | | | |
|--------|--------|--------|--------|--------|--------|
| COL150 | MEL150 | MVE2 | MVJ150 | NPA150 | PIE150 |
| FLO150 | MVA150 | MVF150 | MVK150 | PAL150 | ROC150 |
| MAL150 | MVC150 | MVH150 | NOR150 | PES150 | SOL150 |

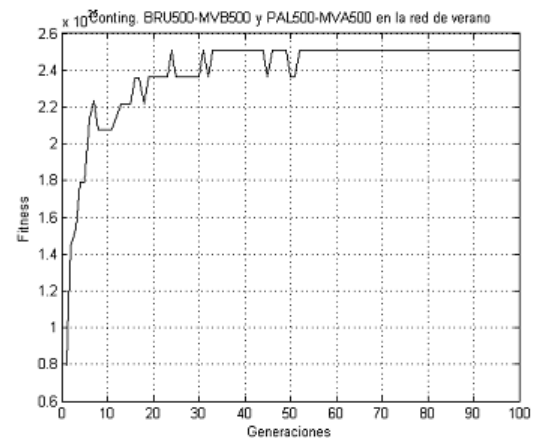
After implementing the solution, the overloading lines are as follows:

| Initial Bus | Final Bus | Current (A) | Overload (%) |
|-------------|-----------|-------------|--------------|
| ACO150 | MVB150 | 195.268 | 37.551 |
| BAY150 | PAL150 | -216.514 | 45.11 |
| BAY150 | TRI150 | 246.611 | 68.526 |
| COL150 | ROS150 | 102.917 | 42.85 |
| COL150 | JLA150 | 128.731 | 31.025 |
| CON150 | COL150 | 231.647 | 64.368 |
| DUR150 | FLO150 | 397.67 | 64.574 |
| EFI150 | SVA150 | 41.026 | 17.082 |
| FBE150 | MER150 | 305.566 | 63.663 |

| | | | |
|--------|--------|----------|--------|
| FLO150 | PRO150 | 397.67 | 64.574 |
| JLA150 | LIB150 | 128.731 | 43.492 |
| LIB150 | EFI150 | 68.2 | 18.951 |
| MER150 | NPA150 | 234.731 | 97.732 |
| NPA150 | CON150 | 234.731 | 56.572 |
| PAL150 | TRI150 | 478.268 | 99.645 |
| PAY150 | YOU150 | 20.069 | 4.837 |
| PRO150 | MVA150 | 397.67 | 64.574 |
| ROD150 | ACO150 | 268.345 | 55.909 |
| ROD150 | MVB150 | 283.141 | 45.805 |
| SAL150 | PAY150 | 185.406 | 38.629 |
| SGU150 | SAL150 | 334.889 | 69.773 |
| SJA150 | FBE150 | 339.493 | 55.127 |
| TER150 | BAY150 | -350.953 | 56.775 |
| TER150 | DUR150 | 461.62 | 64.135 |
| TRI150 | ROD150 | 687.224 | 71.59 |
| SGU500 | SGU150 | 139.378 | 73.154 |
| SJA500 | SJA150 | 101.848 | 53.456 |
| PAL500 | PAL150 | 209.385 | 69.743 |

As can be seen, the most overloaded element, PAL150-TRI150, is a percentage of 99.645%.

The following shows that it took more than 50 generations to reach convergence of the program



PAL500-MVA500 y BRU500-MVB500 double contingency for winter peak

The following table shows the lines that are overloaded and the percentage of overload without load shedding:

| Initial Bus | Final Bus | Current (A) | Overload (%) |
|-------------|-----------|-------------|--------------|
| ACO150 | MVB150 | 1129.246 | 217.163 |
| BAY150 | PAL150 | -1325.66 | 276.196 |
| BAY150 | TRI150 | 620.993 | 172.555 |
| COL150 | ROS150 | 311.871 | 129.85 |
| COL150 | JLA150 | 658.949 | 158.813 |

| | | | |
|--------|--------|----------|---------|
| CON150 | COL150 | 1049.124 | 291.519 |
| DUR150 | FLO150 | 1552.945 | 252.167 |
| EFI150 | SVA150 | 577.152 | 240.302 |
| FBE150 | MER150 | 1044.069 | 217.528 |
| FLO150 | PRO150 | 1435.25 | 233.055 |
| JLA150 | LIB150 | 658.949 | 222.627 |
| LIB150 | EFI150 | 605.369 | 168.213 |
| MER150 | NPA150 | 1131.633 | 471.165 |
| NPA150 | CON150 | 1052.041 | 253.551 |
| PAL150 | TRI150 | 1954.756 | 407.266 |
| PAY150 | YOU150 | 728.021 | 175.459 |
| PRO150 | MVA150 | 1435.25 | 233.055 |
| ROD150 | ACO150 | 1189.558 | 247.84 |
| ROD150 | MVB150 | 1421.159 | 229.905 |
| SAL150 | PAY150 | 914.647 | 190.563 |
| SGU150 | SAL150 | 1071.26 | 223.193 |
| SJA150 | FBE150 | 1250.631 | 203.077 |
| SVA150 | MVC150 | 462.474 | 111.46 |
| TER150 | BAY150 | -1085.72 | 175.64 |
| TER150 | DUR150 | 1619.262 | 224.971 |
| TRI150 | ROD150 | 2534.399 | 264.016 |
| YOU150 | TER150 | 481.332 | 116.005 |
| SGU500 | SGU150 | 347.702 | 182.496 |
| SJA500 | SJA150 | 375.189 | 196.923 |
| PAL500 | PAL150 | 985.343 | 328.205 |

| | | | |
|--------|--------|----------|--------|
| EFI150 | SVA150 | 108.539 | 45.191 |
| FBE150 | MER150 | 234.055 | 48.764 |
| FLO150 | PRO150 | 365.437 | 59.34 |
| JLA150 | LIB150 | 136.755 | 46.203 |
| LIB150 | EFI150 | 136.755 | 38 |
| MER150 | NPA150 | 218.476 | 90.964 |
| NPA150 | CON150 | 138.884 | 33.472 |
| PAL150 | TRI150 | 479.917 | 99.989 |
| PAY150 | YOU150 | 46.01 | 11.089 |
| PRO150 | MVA150 | 365.437 | 59.34 |
| ROD150 | ACO150 | 324.216 | 67.549 |
| ROD150 | MVB150 | 397.691 | 64.336 |
| SAL150 | PAY150 | 232.636 | 48.469 |
| SGU150 | SAL150 | 389.249 | 81.099 |
| SJA150 | FBE150 | 440.618 | 71.547 |
| SVA150 | MVC150 | -6.139 | 1.48 |
| TER150 | BAY150 | -367.108 | 59.388 |
| TER150 | DUR150 | 549.449 | 76.337 |
| TRI150 | ROD150 | 719.778 | 74.981 |
| YOU150 | TER150 | -97.537 | 23.507 |
| SGU500 | SGU150 | 143.098 | 75.107 |
| SJA500 | SJA150 | 132.185 | 69.379 |
| PAL500 | PAL150 | 212.968 | 70.937 |

As can be seen, the most overloaded element, PAL150-TRI150, is a percentage of 99,989%.

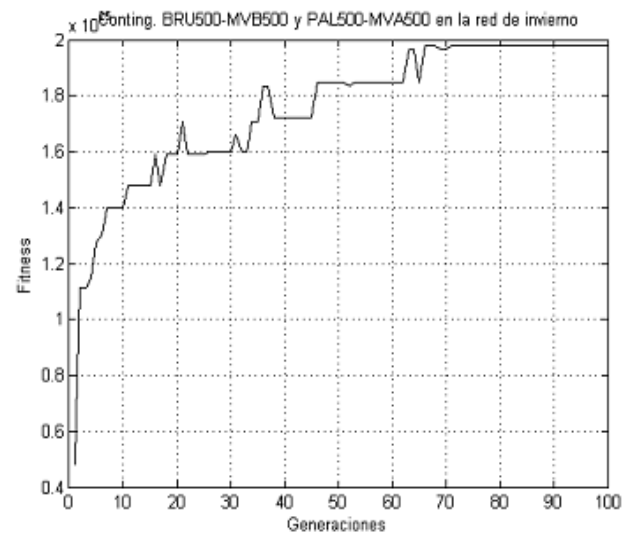
The following figure shows that it took more than 70 generations to reach convergence of the program.

To clear the overloads of the network the program calculates that 1057 MW to be disconnected by shedding the following (all at 150kV):

| | | | | |
|--------|--------|--------|--------|--------|
| ACO150 | MAL150 | MVG150 | PAN150 | ROD150 |
| COL150 | MVC150 | MVH150 | PAZ150 | ROS150 |
| CON150 | MVE2 | MVR1 | PIE150 | SOL150 |
| LIB150 | MVF150 | NOR150 | RIV150 | TRI150 |
| | | | | TYT150 |

After implementing the solution, the overloading lines are as follows:

| Initial Bus | Final Bus | Current (A) | Overload (%) |
|-------------|-----------|-------------|--------------|
| ACO150 | MVB150 | 324.216 | 62.349 |
| BAY150 | PAL150 | -225.918 | 47.069 |
| BAY150 | TRI150 | 239.861 | 66.65 |
| COL150 | ROS150 | 2.129 | 0.887 |
| COL150 | JLA150 | 136.755 | 32.959 |
| CON150 | COL150 | 138.884 | 38.592 |
| DUR150 | FLO150 | 483.132 | 78.451 |



PAL500-MVA500 y MVB500-MVA500 double contingency for winter peak

The following table shows the lines that are overloaded and the percentage of overload without load shedding:

| Initial Bus | Final Bus | Current (A) | Overload (%) |
|-------------|-----------|-------------|--------------|
| MER150 | NPA150 | 291.092 | 121.198 |
| MVB150 | MVL150 | 894.153 | 124.162 |
| MVB150 | MVA150 | 1267.857 | 132.077 |
| MVD150 | MVE2 | 776.173 | 107.78 |
| COL150 | JLA150 | 136.755 | 32.959 |
| MVB500 | MVB150 | 975.533 | 140.082 |

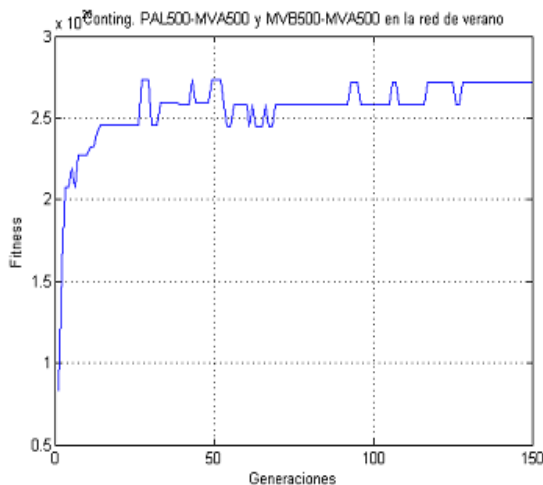
To clear the overloads of the network the program calculates that 347 MW to be disconnected by shedding the following (all at 150kV):

| | | | |
|--------|--------|--------|--------|
| COL150 | MVG150 | PES150 | TRI150 |
| MAL150 | MVL150 | ROC150 | |
| MVB150 | MVR1 | ROD150 | |

After implementing the solution, the overloading lines are as follows:

| Initial Bus | Final Bus | Current (A) | Overload (%) |
|-------------|-----------|-------------|--------------|
| MER150 | NPA150 | 186.315 | 77.574 |
| MVB150 | MVL150 | 636.31 | 88.358 |
| MVB150 | MVA150 | 895.24 | 93.26 |
| MVD150 | MVE2 | 528.031 | 73.323 |
| COL150 | JLA150 | 136.755 | 32.959 |
| MVB500 | MVB150 | 694.265 | 99.693 |

As can be seen, the most overloaded element, MVB500-MVB150, is a percentage of 99,693%. The following figure shows that it took more than 120 generations to reach convergence of the program.



PAL500-MVA500 y MVB500-MVA500 double contingency for winter peak

The following table shows the lines that are overloaded and the percentage of overload without load shedding:

| Initial Bus | Final Bus | Current (A) | Overload (%) |
|-------------|-----------|-------------|--------------|
| MER150 | NPA150 | 293.17 | 122.064 |
| MVB150 | MVL150 | 1077.838 | 149.669 |
| MVB150 | MVA150 | 1451.034 | 151.159 |
| MVD150 | MVE2 | 913.822 | 126.894 |
| MVI150 | MVM1 | -999.556 | 107.745 |
| MVM1 | MVA150 | -999.556 | 107.745 |
| PAL150 | TRI150 | 495.758 | 103.289 |
| SGU150 | SAL150 | 549.868 | 114.563 |
| SGU500 | SGU150 | 191.284 | 100.398 |
| MVB500 | MVB150 | 1140.638 | 163.791 |

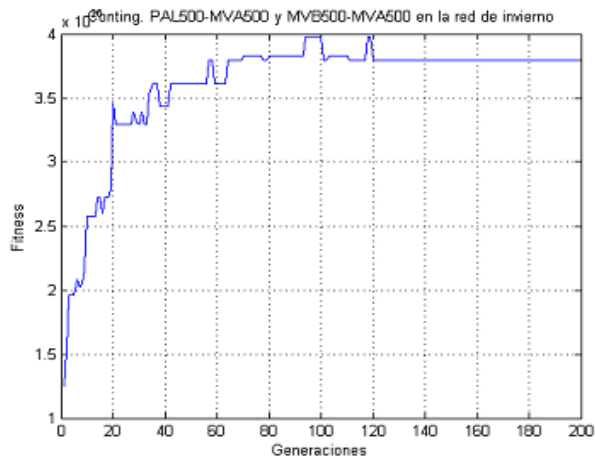
To clear the overloads of the network the program calculates that 529 MW to be disconnected by shedding the following (all at 150kV):

| | | |
|--------|--------|--------|
| ACO150 | MVC150 | PAN150 |
| EFI150 | MVE2 | PIE150 |
| MAL150 | MVF150 | STE150 |

After implementing the solution, the overloading lines are as follows:

| Initial Bus | Final Bus | Current (A) | Overload (%) |
|-------------|-----------|-------------|--------------|
| MER150 | NPA150 | 161.021 | 67.042 |
| MVB150 | MVL150 | 706.96 | 98.169 |
| MVB150 | MVA150 | 950.007 | 98.965 |
| MVD150 | MVE2 | 597.457 | 82.963 |
| MVI150 | MVM1 | -776.358 | 80.876 |
| MVM1 | MVA150 | 312.966 | 65.205 |
| PAL150 | TRI150 | 414.204 | 86.298 |
| SGU150 | SAL150 | 150.585 | 79.036 |
| SGU500 | SGU150 | 696.269 | 99.981 |

As can be seen, the most overloaded element, SGU500-SGU150, is a percentage of 99,981%. The following figure shows that it took more than 120 generations to reach convergence of the program.



VIII. CONCLUSIONS

In all cases the solution leaves a network which has no overloaded elements, and most loaded lines are very close to 100% capacity. While these two features are not sufficient conditions to ensure that the solution found corresponds to the optimal load shedding, are strictly necessary for the solution to be valid and were the premises of the project.

The result is achieved in a relatively short time (depending on the computer varies between 5 and 8 minutes). An exhaustive search program trying all possibilities would take months to run.

Part of the program's success is attributed to the dedication to the implementation of the fitness function in conjunction with the final adjustment to be made to the result found by genetic algorithms.